

1. We observe that the first three joint axes always intersect at the common point $O_0 = O_1 = O_2$. A closed-form inverse kinematic solution is therefore guaranteed. We use the decoupling principle to arrive at the solution. Since the location of the co-intersection point $O_0 = O_1 = O_2$ as seen from the end-effector frame of reference (frame 6) does not change with motion of the first three joints, the position of $O_0 = O_1 = O_2$ expressed in the end-effector frame (frame 6), ${}^6\mathbf{p}_0 = {}^6\mathbf{p}_1 = {}^6\mathbf{p}_2$, is a function of the last three joint coordinates (joints 4, 5, and 6) only. This position ${}^6\mathbf{p}_0$ is directly obtained from the task description ${}^0\mathbf{T}_6$ using:

$${}^6\mathbf{p}_0 = -{}^0\mathbf{R}_6^T {}^0\mathbf{p}_6, \quad (1)$$

i.e., ${}^6\mathbf{p}_0$ is the last column of the inverse of ${}^0\mathbf{T}_6$. We express ${}^6\mathbf{p}_0$ in terms of the last three joint coordinates by taking the fourth column of ${}^6\mathbf{T}_2 = \mathbf{A}_6^{-1}\mathbf{A}_5^{-1}\mathbf{A}_4^{-1}\mathbf{A}_3^{-1}$:

$${}^6\mathbf{p}_0 = {}^6\mathbf{p}_2 = \begin{pmatrix} p_x^* \\ p_y^* \\ p_z^* \end{pmatrix} = \begin{pmatrix} -c_6(L_1c_{45} + L_2c_5) \\ s_6(L_1c_{45} + L_2c_5) \\ L_1s_{45} + L_2s_5 - L_3 \end{pmatrix} \quad (2)$$

The decoupled system consists of the decoupled task (Equation (2)) and decoupled set of joint coordinates 4, 5 and 6 (Equation (1)).

The nonlinear system (2) represents a low-order system of three equations in three unknowns $(\theta_4, \theta_5, \theta_6)$, for which a closed-form solution is guaranteed:

$$\theta_4 = \text{ATAN2} \left(\frac{I_4 \sqrt{4L_1^2L_2^2 - (p_x^{*2} + p_y^{*2} + (p_z^* + L_3)^2 - L_1^2 - L_2^2)^2}}{p_x^{*2} + p_y^{*2} + (p_z^* + L_3)^2 - L_1^2 - L_2^2} \right) \quad (3)$$

where $4L_1^2L_2^2 - (p_x^{*2} + p_y^{*2} + (p_z^* + L_3)^2 - L_1^2 - L_2^2)^2$ must be ≥ 0 ; otherwise, the end-effector position is unreachable.

$$\theta_6 = \text{ATAN2} \left(\frac{I_6 p_y^*}{-I_6 p_x^*} \right) \quad (4)$$

$$\theta_5 = \text{ATAN2} \left(\frac{(L_1c_4 + L_2)(p_z^* + L_3) - L_1s_4(-p_x^*c_6 + p_y^*s_6)}{(L_1c_4 + L_2)(-p_x^*c_6 + p_y^*s_6) + L_1s_4(p_z^* + L_3)} \right) \quad (5)$$

where $I_4 = \pm 1$ in (3) and $I_6 = \pm 1$ in (4). Having solved for $(\theta_4, \theta_5, \theta_6)$, we now compute

$${}^3\mathbf{T}_6 = \mathbf{A}_4\mathbf{A}_5\mathbf{A}_6. \quad (6)$$

The orientation of frame 3 in frame 0 is then computed from the the task description:

$${}^0\mathbf{T}_3 = {}^0\mathbf{T}_6 {}^3\mathbf{T}_6^{-1}. \quad (7)$$

${}^0\mathbf{T}_3$ is a function of the first three joint coordinates only. Having solved for $(\theta_4, \theta_5, \theta_6)$ to satisfy the end-effector position, we now solve for $(\theta_1, \theta_2, \theta_3)$ to satisfy the end-effector orientation by taking the rotation matrix part of ${}^0\mathbf{T}_3 = \mathbf{A}_1\mathbf{A}_2\mathbf{A}_3$ only:

$${}^0\mathbf{R}_3 = \begin{pmatrix} N_x & O_x & A_x \\ N_y & O_y & A_y \\ N_z & O_z & A_z \end{pmatrix} = \begin{pmatrix} c_1c_2c_3 + s_1s_3 & -c_1c_2s_3 + s_1c_3 & -c_1s_2 \\ s_1c_2c_3 - c_1s_3 & -s_1c_2s_3 - c_1c_3 & -s_1s_2 \\ -s_2c_3 & s_2s_3 & -c_2 \end{pmatrix} \quad (8)$$

From the A_z elements we have

$$\theta_2 = \text{ATAN2} \left(\frac{I_2 \sqrt{1 - A_z^2}}{-A_z} \right), \quad (9)$$

where $I_2 = \pm 1$. From the A_x , A_y , N_z , and O_z elements of (8), and for $A_z^2 \neq 1$, we have:

$$\theta_1 = \text{ATAN2} \left(\frac{-I_2 A_y}{-I_2 A_x} \right), \quad (10)$$

$$\theta_3 = \text{ATAN2} \left(\frac{I_2 O_z}{-I_2 N_z} \right). \quad (11)$$

In general, there are eight inverse kinematic solutions corresponding to $I_4 = \pm 1$, $I_6 = \pm 1$, and $I_2 = \pm 1$.

If $A_z = \pm 1$, θ_1 and θ_3 describe the same rotation and cannot be computed separately; one degree-of-freedom is lost.

$$A_z = -1 \longleftrightarrow \begin{cases} \theta_2 = 0^\circ \\ \theta_1 - \theta_3 = \text{ATAN2} \left(\frac{O_x}{N_x} \right) \end{cases} \quad (12)$$

$$A_z = 1 \longleftrightarrow \begin{cases} \theta_2 = 180^\circ \\ \theta_1 + \theta_3 = \text{ATAN2} \left(\frac{O_x}{-N_x} \right) \end{cases} \quad (13)$$

Thus when $A_z = \pm 1$, there are an infinite number of solutions.